

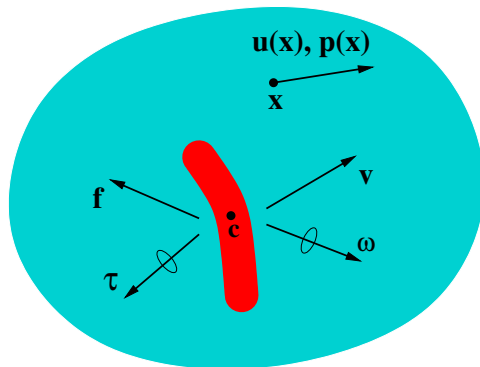
# On the Stokesian hydrodynamics of rigid bodies

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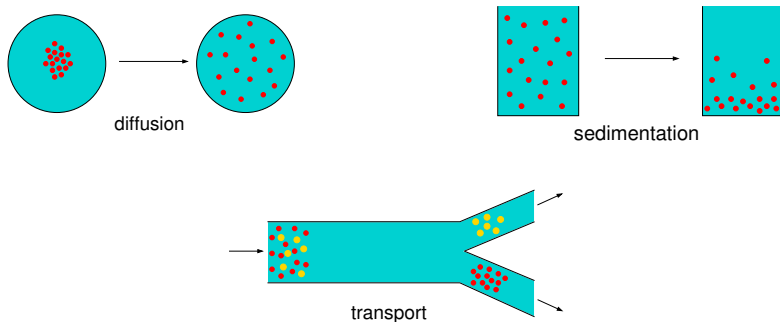
# Introduction

**Goal.** To characterize the hydrodynamic mobility properties of a rigid body in a viscous fluid under Stokes flow conditions.



# Introduction

**Motivation.** Hydrodynamic mobility properties of a body play a central role in models of diffusion, sedimentation and transport.



**Applications.** Microfluidic devices for separation and mixing of particles; magnetic microswimmers; free-soln DNA sequencing.

# Outline

Introduction

Background

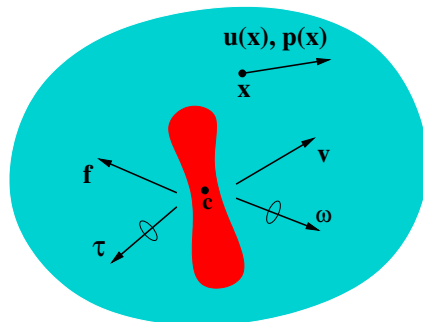
Mobility coefficient

Transport velocity

# Background

## Background

**Setup.** Consider slow, quasi-static motion of a body in an infinite viscous fluid.



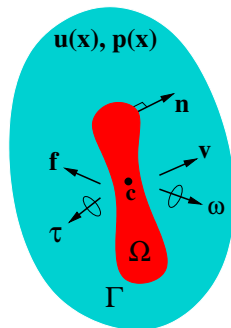
- $u(x), p(x)$  velocity and pressure fields in fluid.
- $f, \tau$  external force and torque on body.
- $v, \omega$  linear and angular velocity of body.
- $c$  reference point for velocities, loads.

## Background

**Fluid-body equations.** Stokes system in exterior domain for fluid; balance of external and hydrodynamic loads for body.

$$\begin{aligned} \Delta u &= \nabla p && \text{in } \mathbb{R}^3 \setminus \Omega \\ \nabla \cdot u &= 0 && \text{in } \mathbb{R}^3 \setminus \Omega \\ u &= v + \omega \times (x - c) && \text{on } \Gamma = \partial\Omega \\ u, p &\rightarrow u_\infty, p_\infty && \text{as } |x| \rightarrow \infty \end{aligned}$$

$$\begin{aligned} f + \int_{\Gamma} \sigma[u, p] n \, dA &= 0 \\ \tau + \int_{\Gamma} (x - c) \times \sigma[u, p] n \, dA &= 0 \end{aligned}$$



Here  $\sigma[u, p] = 2 \text{sym}(\nabla u) - pl$  is stress field in fluid; all quantities non-dimensional.

## Background

**Basic BVP.** Given  $(u_\infty, p_\infty, f, \tau)$  determine  $(u, p, v, \omega)$ .

$$\begin{aligned}
 \Delta u &= \nabla p && \text{in } \mathbb{R}^3 \setminus \Omega \\
 \nabla \cdot u &= 0 && \text{in } \mathbb{R}^3 \setminus \Omega \\
 u &= v + \omega \times (x - c) && \text{on } \Gamma = \partial\Omega \\
 u, p &\rightarrow u_\infty, p_\infty && \text{as } |x| \rightarrow \infty \\
 f + \int_\Gamma \sigma[u, p] n \, dA &= 0 \\
 \tau + \int_\Gamma (x - c) \times \sigma[u, p] n \, dA &= 0
 \end{aligned}$$

Assume  $\Gamma$  is closed, bounded, non-self-intersecting and class  $C^{1,\alpha}$ ;  
well-developed analysis/numerics based on potential theory.



## Background

**Stokes matrices.** When conditions at infinity are zero, there is an invertible linear map between  $(\mathbf{v}, \boldsymbol{\omega}) \in \mathbb{R}^6$  and  $(\mathbf{f}, \boldsymbol{\tau}) \in \mathbb{R}^6$ .

$$\begin{aligned} \Delta u &= \nabla p && \text{in } \mathbb{R}^3 \setminus \Omega \\ \nabla \cdot u &= 0 && \text{in } \mathbb{R}^3 \setminus \Omega \\ u &= \mathbf{v} + \boldsymbol{\omega} \times (\mathbf{x} - \mathbf{c}) && \text{on } \Gamma = \partial\Omega \\ u, p &\rightarrow 0, 0 && \text{as } |\mathbf{x}| \rightarrow \infty \end{aligned}$$

$$\begin{aligned} \mathbf{f} + \int_{\Gamma} \sigma[u, p] \mathbf{n} \, dA &= 0 \\ \boldsymbol{\tau} + \int_{\Gamma} (\mathbf{x} - \mathbf{c}) \times \sigma[u, p] \mathbf{n} \, dA &= 0 \end{aligned}$$

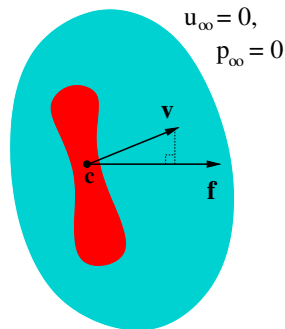
$$(\mathbf{v}, \boldsymbol{\omega}) = M(\mathbf{f}, \boldsymbol{\tau}), \quad M = \begin{bmatrix} M_1 & M_3 \\ M_2 & M_4 \end{bmatrix}, \quad M = M^T > 0$$

$$(\mathbf{f}, \boldsymbol{\tau}) = L(\mathbf{v}, \boldsymbol{\omega}), \quad L = \begin{bmatrix} L_1 & L_3 \\ L_2 & L_4 \end{bmatrix}, \quad L = L^T > 0$$

# Mobility coefficient

## Mobility coefficient

**Definition.** Consider body subject to a unit force in fluid at rest at infinity; consider velocity along force, average over orientations.



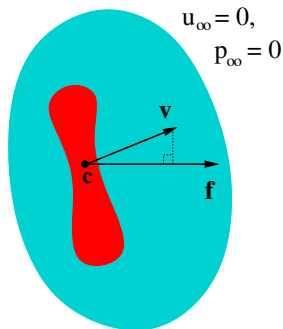
## Mobility coefficient

**Definition.** Consider body subject to a unit force in fluid at rest at infinity; consider velocity along force, average over orientations.

$v, f$  velocity, force at  $c$

$v_f = v \cdot f$  component along  $f$

$\mathcal{M} = \text{avg}_{f \in S^2} v_f$  average over  $|f| = 1$

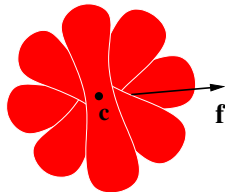
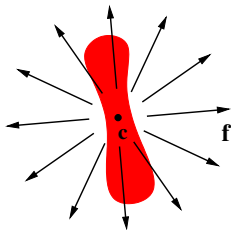


$\mathcal{M}$  is called the mobility coefficient; it is the average velocity imparted to the body along an imposed unit force.

## Mobility coefficient

**Interpretation.**  $\mathcal{M}$  is average velocity along a unit force when either force or body orientation are fixed, and other is randomized.

$$\mathcal{M} = \text{avg}_{f \in S^2} v_f$$



$\mathcal{M}$  naturally arises in transport problems; proportional to diffusion, sedimentation coefficients.

## Mobility coefficient

**Characterization.** The mobility coefficient  $\mathcal{M}$  can be expressed in terms of the Stokes matrix  $M$ .

$$(v, \omega) = M(f, \tau), \quad \tau = 0 \quad \implies \quad v = M_1 f$$

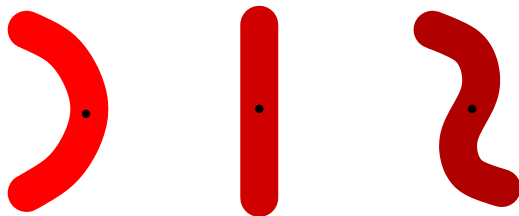
$$v_f = v \cdot f = f \cdot M_1 f$$

$$\mathcal{M} = \mathop{\text{avg}}_{f \in S^2} v_f = \frac{1}{3} \text{tr}(M_1)$$

Can compute using boundary-element techniques; but there are various natural questions for analysis.

## Mobility coefficient

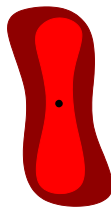
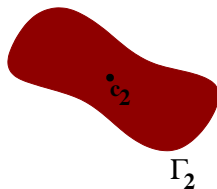
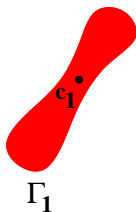
**Questions.** How does  $\mathcal{M}$  vary among bodies of different shape?  
Are there simple criteria for ordering shapes by  $\mathcal{M}$ ?



## Mobility coefficient

**Inclusion monotonicity theorem.** [Hill & Power; and others]. Let  $\Gamma_1$  and  $\Gamma_2$  be body surfaces, with reference points  $c_1$  and  $c_2$ . If  $\Gamma_1$  can be enclosed by  $\Gamma_2$ , with  $c_1$  and  $c_2$  superimposed, then

$$\mathcal{M}_1 \geq \mathcal{M}_2.$$





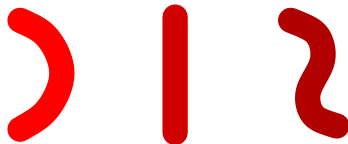
# Mobility coefficient

## Remarks.

- Inclusion theorem implies

“smaller body”  $\implies$  “higher mobility”.

- Result provides little insight for filament-type bodies



## Mobility coefficient

**Inverse chord theorem.** Let  $\Gamma$  be a body surface with reference point  $c$  at its centroid. Then

$$2 \min_{\mathbf{x}, \mathbf{y} \in \Gamma} \frac{1}{|\mathbf{x} - \mathbf{y}|} \leq 6\pi\mathcal{M} \leq \text{avg}_{\mathbf{x}, \mathbf{y} \in \Gamma} \frac{1}{|\mathbf{x} - \mathbf{y}|}.$$



## Mobility coefficient

### Remarks.

- Theorem implies geometric inequality for arbitrary surfaces

$$2 \min_{x,y \in \Gamma} \frac{1}{|x-y|} \leq \text{avg}_{x,y \in \Gamma} \frac{1}{|x-y|}.$$

- Theorem implies existence of a characteristic chord length  $|x_* - y_*|$  such that

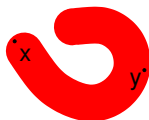
$$6\pi\mathcal{M} = \frac{1}{|x_* - y_*|}.$$

# Mobility coefficient

## Remarks.

- Lower bound in theorem suggests the heuristic

“higher  $\min_{x,y \in \Gamma} \frac{1}{|x-y|}$ ”  $\implies$  “higher mobility”.



higher



# Mobility coefficient

## Remarks.

- Upper bound in theorem suggests the heuristic

“lower  $\text{avg}_{x,y \in \Gamma} \frac{1}{|x-y|}$ ”  $\implies$  “lower mobility”.

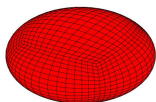


lower

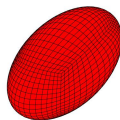


## Mobility coefficient

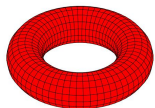
**Example bounds.**  $2 \min_{x,y \in \Gamma} \frac{1}{|x-y|} \leq 6\pi\mathcal{M} \leq \text{avg}_{x,y \in \Gamma} \frac{1}{|x-y|}$ .



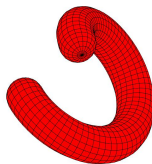
$$1.000 \leq 1.209 \leq 1.220$$



$$1.000 \leq 1.521 \leq 1.533$$



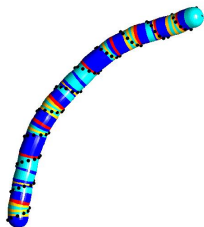
$$0.750 \leq 0.966 \leq 0.992$$



$$0.712 \leq 0.892 \leq 0.921$$

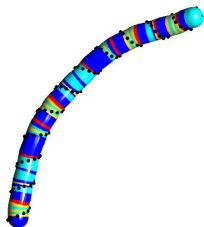
## Mobility coefficient

**Example application.** Mobility coefficient  $\mathcal{M}$  can be used to estimate structural features of molecular bodies.



## Mobility coefficient

**Example application.** Mobility coefficient  $\mathcal{M}$  can be used to estimate structural features of molecular bodies.



If DNA is modeled as a filament, what would be its effective radius in solution?

Can estimate radius by fitting computed values of  $\mathcal{M}$  to experimental data.



## Mobility coefficient

**Geometric models.** For comparison, consider two different models for a DNA sequence  $S$ ; each has uniform radius  $r$ .

Straight model:

axial length determined by  
number of basepairs in  $S$ .



## Mobility coefficient

**Geometric models.** For comparison, consider two different models for a DNA sequence  $S$ ; each has uniform radius  $r$ .

Straight model:

axial length determined by  
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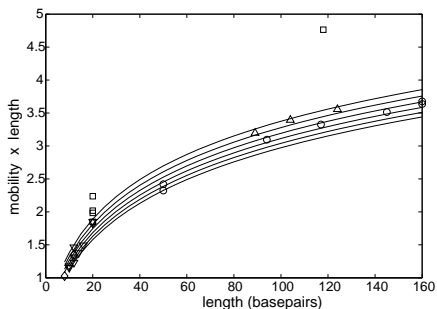
Curved model:

axial length, curvature determined  
by sequence composition of  $S$ .



# Mobility coefficient

## Results for straight model.



*Curves:* numerics with  $r = 10, 11, \dots, 15 \text{ \AA}$  from top to bottom.

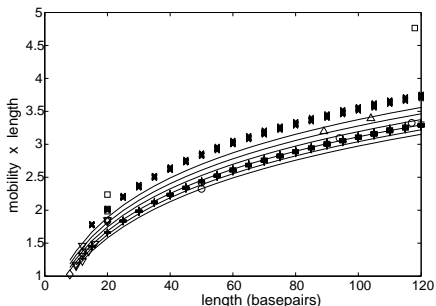
*Open circles, triangles:* data from sedimentation, diffusion.

*Open squares:* data from electrophoresis.

*Estimate of hydrated radius:*  $r = 10 - 15 \text{ \AA}$ .

# Mobility coefficient

## Results for curved model.



*Curves:* numerics on straight model as before.

*Open symbols:* experimental data as before.

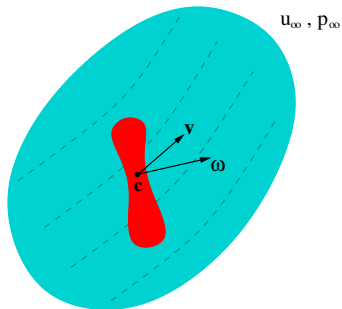
*Crosses, pluses:* numerics on curved model w/ $r = 10$ ,  $r = 15\text{\AA}$ .

*Revised estimate of hydrated radius:*  $r = 12 - 17\text{\AA}$ .

# Transport velocity

## Transport velocity

**Definition.** Consider body in an ambient fluid flow; let flow freely carry body with no external forces acting.

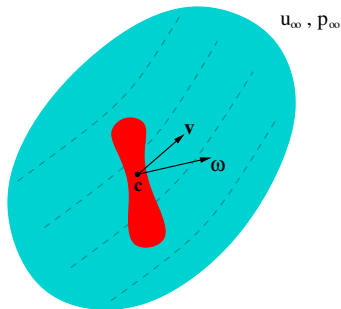


## Transport velocity

**Definition.** Consider body in an ambient fluid flow; let flow freely carry body with no external forces acting.

$u_\infty, p_\infty$  ambient flow fields

$v, \omega$  body velocities



$(v, \omega)$  are called transport velocities; they are imparted to the body as it is carried by the fluid.

## Transport velocity

**BVP formulation.** Given  $(u_\infty, p_\infty)$  we can determine  $(v, \omega)$  and disturbed flow  $(u, p)$  via the following

$$\begin{aligned} \Delta u &= \nabla p && \text{in } \mathbb{R}^3 \setminus \Omega \\ \nabla \cdot u &= 0 && \text{in } \mathbb{R}^3 \setminus \Omega \\ u &= v + \omega \times (x - c) && \text{on } \Gamma = \partial\Omega \\ u, p &\rightarrow u_\infty, p_\infty && \text{as } |x| \rightarrow \infty \end{aligned}$$

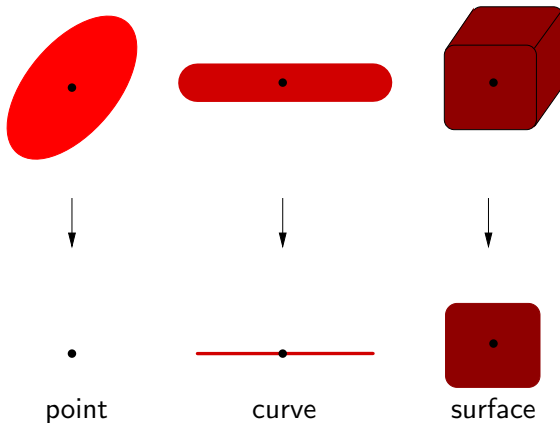
$$\begin{aligned} \int_\Gamma \sigma[u, p] n \, dA &= 0 \\ \int_\Gamma (x - c) \times \sigma[u, p] n \, dA &= 0 \end{aligned}$$

Can characterize  $(v, \omega)$  in terms of Stokes matrix  $M$  and loads  $(f_\infty, \tau_\infty)$  associated with ambient flow.



## Transport velocity

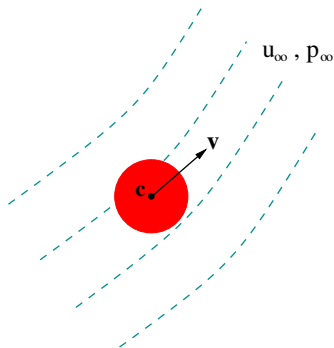
**Questions.** How do transport velocities depend on body shape?  
What happens in limiting cases as body volume tends to zero?



# Transport velocity

**Sphere limit theorem.** Consider a sphere of radius  $r$  and center  $c$ . Then

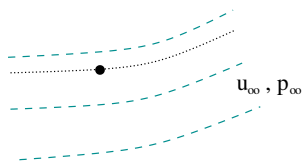
$$\lim_{r \downarrow 0} v = u_{\infty}(c).$$



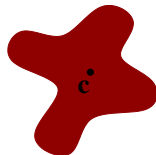
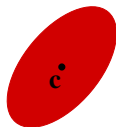
# Transport velocity

## Remarks.

- Theorem implies limiting sphere would follow streamlines.



- Theorem extends to zero-radius limit of more general shapes.

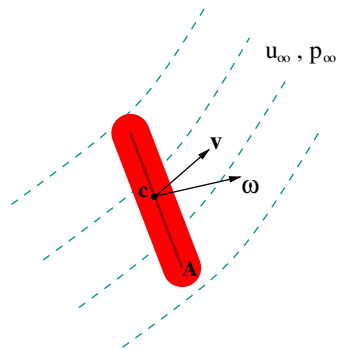


## Transport velocity

**Cylinder limit theorem.** Consider a cylinder with axis  $A$  and radius  $r$ , with capped ends, and reference point  $c$  at its centroid. Then

$$\ell_A \cdot \lim_{r \downarrow 0} v = \int_A u_\infty ds$$

$$I_A \cdot \lim_{r \downarrow 0} \omega = \int_A (x - c) \times u_\infty ds$$

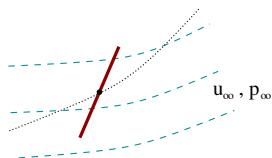


where  $\ell_A$  and  $I_A$  are the length and second-moment matrix for the line segment  $A$ .

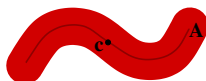
# Transport velocity

## Remarks.

- Theorem implies limiting cylinder may not follow streamlines.



- Theorem extends to zero-radius limit of general tubular shapes.



# Thank You